

# Tensile Testing for Sheet Metal Formability

---

Daniel J. Schaeffler, Ph.D.

President, Engineering Quality Solutions, Inc., [www.EQSgroup.com](http://www.EQSgroup.com)

Chief Content Officer, 4M Partners, LLC, [www.Learning4M.com](http://www.Learning4M.com)

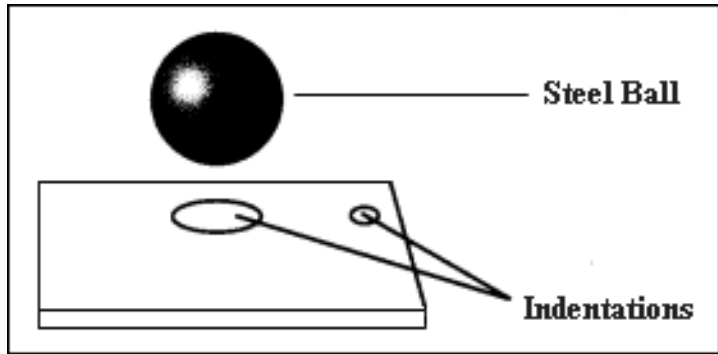
May 2017



splits  
stress  
failure  
formability  
YTE N-value TYE cracking  
strain  
tensile dogbone yield  
uniform elongation necking  
properties strain hardening



# Hardness



Resistance to Permanent Indentation  
Quick and Easy

Test Procedure Dependent  
Poor Indicator of Formability



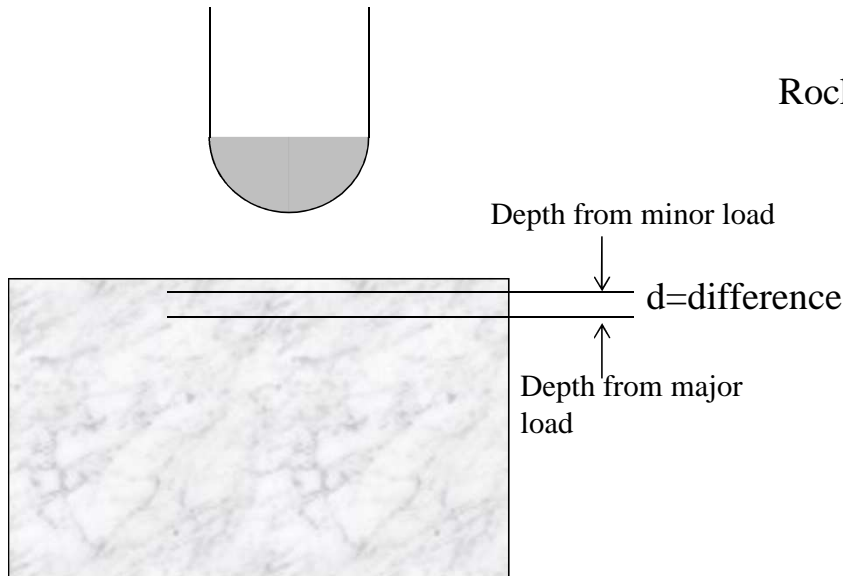
# Hardness

Mohs hardness	Mineral	Chemical formula	Absolute hardness
1	Talc	$Mg_3Si_4O_{10}(OH)_2$	1
2	Gypsum	$CaSO_4 \cdot 2H_2O$	3
3	Calcite	$CaCO_3$	9
4	Fluorite	$CaF_2$	21
5	Apatite	$Ca_5(PO_4)_3(OH^-, Cl^-, F^-)$	48
6	Orthoclase Feldspar	$KAlSi_3O_8$	72
7	Quartz	$SiO_2$	100
8	Topaz	$Al_2SiO_4(OH^-, F^-)_2$	200
9	Corundum	$Al_2O_3$	400
10	Diamond	C	1600



# Schematic of Rockwell Testing resistance to indentation

HRB: 1/16" diameter ball



$$\text{Rockwell B Hardness} = 130 - \frac{d}{0.002 \text{ mm}}$$

$$\text{HRB } 80 = 0.10 \text{ mm}$$

$$\text{HRB } 65 = 0.13 \text{ mm}$$

$$\text{HRB } 50 = 0.16 \text{ mm}$$

(human hair  $\approx 0.10\text{mm}$ )

One Rockwell point =

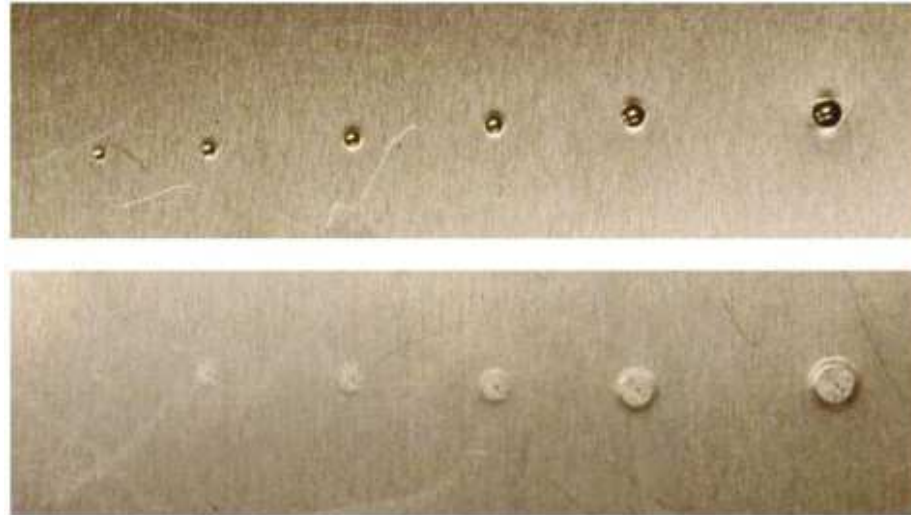
2 microns = 0.00008 inch



# Anvil Effect

Indentation depth  $< 10\%$  of sample thickness

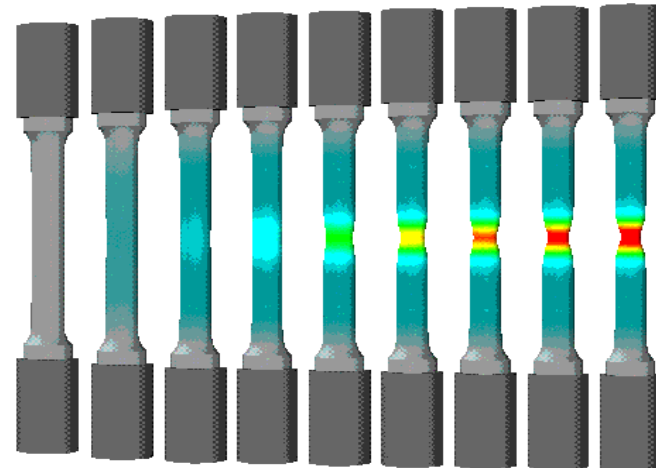
If not, then risk of shiny spot (burnish) on other surface



Zhang, Dhaigude, and Wang, *The Anvil Effect in the Spherical Indentation Testing on Sheet Metals*, *Procedia Manufacturing* Volume 1, 2015, Pages 828–839, doi: 10.1016/j.promfg.2015.09.072  
[https://www.researchgate.net/publication/283958501\\_The\\_Anvil\\_Effect\\_in\\_the\\_Spherical\\_Indentation\\_Testing\\_on\\_Sheet\\_Metals](https://www.researchgate.net/publication/283958501_The_Anvil_Effect_in_the_Spherical_Indentation_Testing_on_Sheet_Metals)



# Tensile Testing





# Definitions

---

## Strength (stress)

= Resistance to Deformation

= Force / Area

## Strain

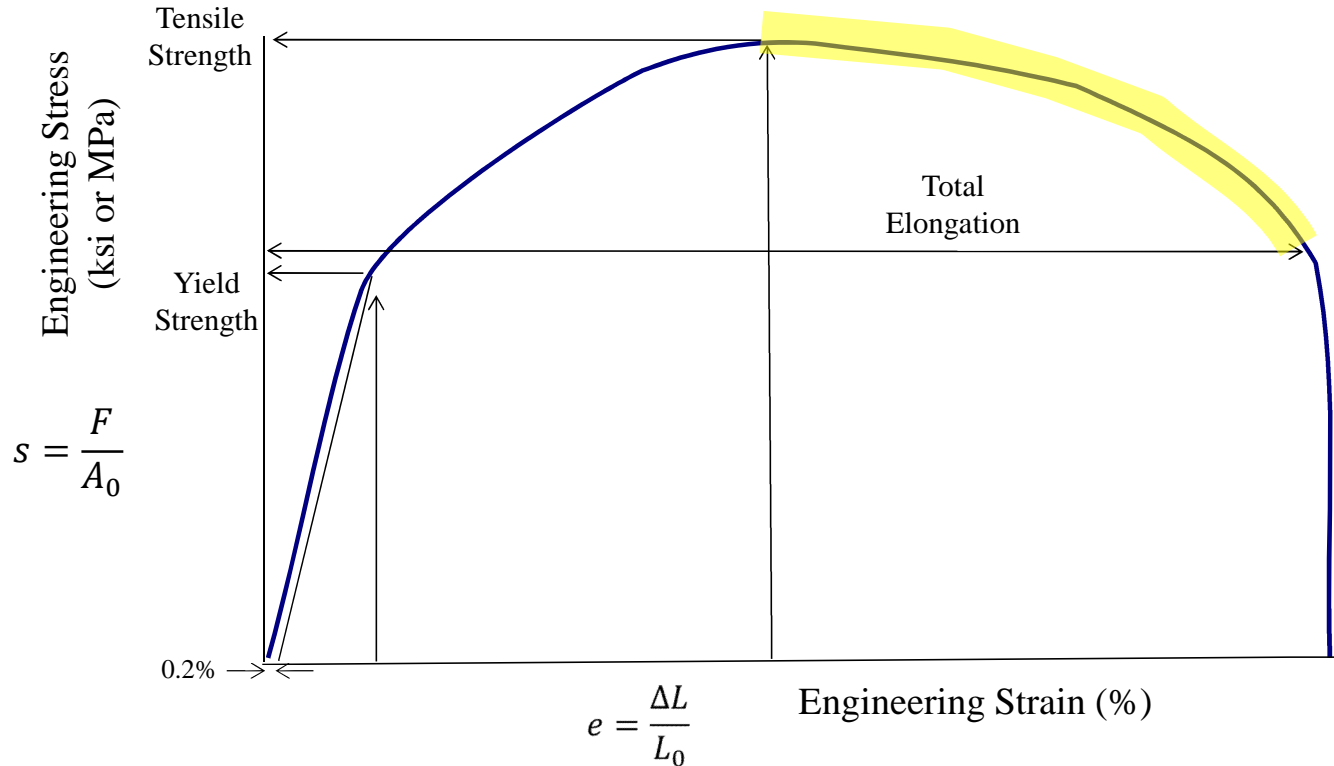
= % Displacement

= Change in length / Original length



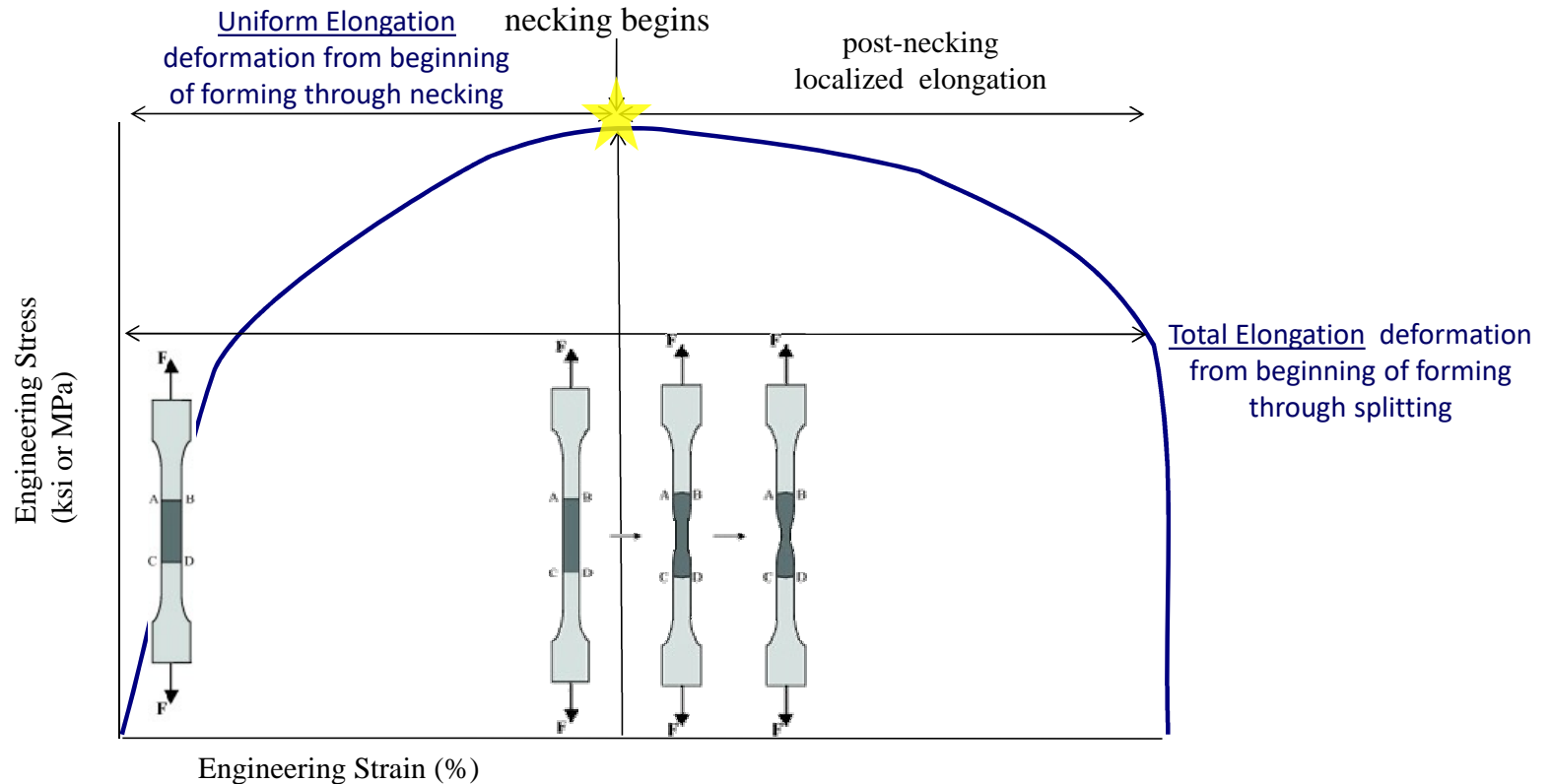


# Tensile Testing



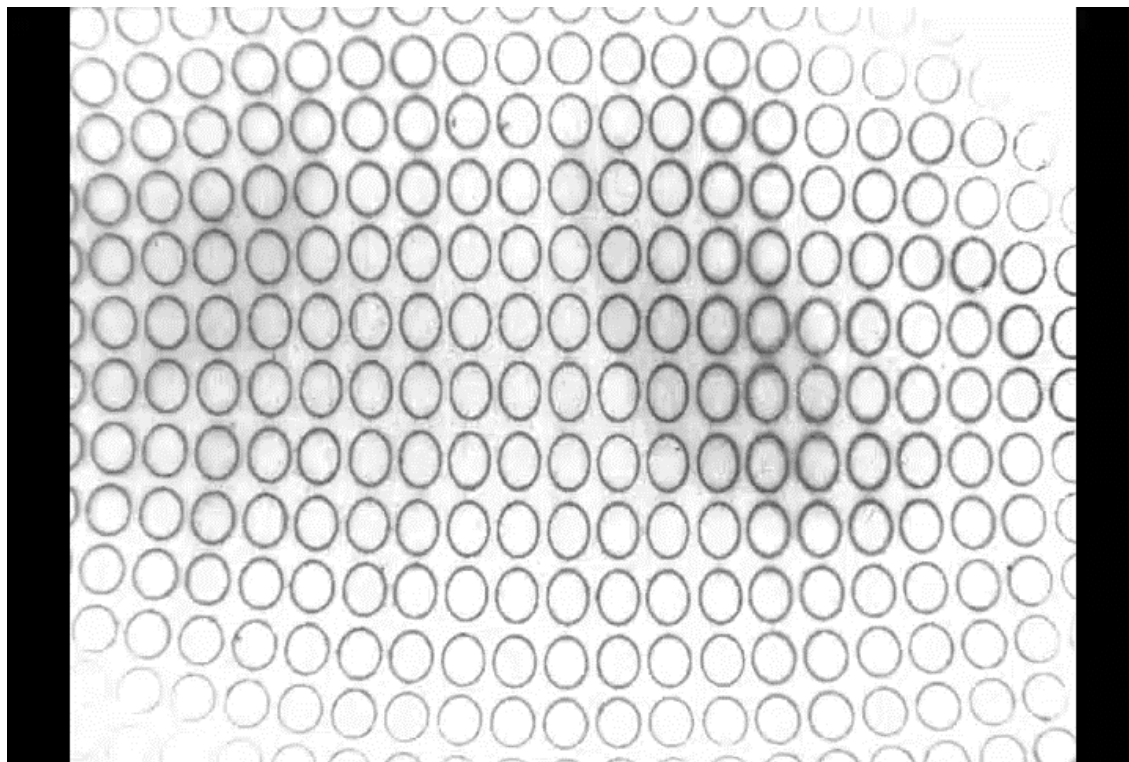


# Elongation: Total vs Uniform





# Necking and Fracture





# Tensile Testing

## Engineering Stress/Strain vs True Stress/Strain

$$\text{Engineering Stress} = s = \frac{F}{A_0} = \frac{\text{Force}}{\text{Initial Cross Sectional Area}}$$

$$\text{True Stress} = \sigma = \frac{F}{A_i} = \frac{\text{Force}}{\text{Instantaneous Cross Sectional Area}}$$

$$\text{Engineering Strain} = e = \frac{L_f - L_0}{L_0} = \frac{\Delta L}{L_0} = \frac{\text{Change in Length}}{\text{Initial Gauge Length}}$$

$$\text{True Strain} = \epsilon = \ln \left\{ \frac{L_i}{L_0} \right\} = \frac{\text{Instantaneous Change in Length}}{\text{Initial Gauge Length}}$$

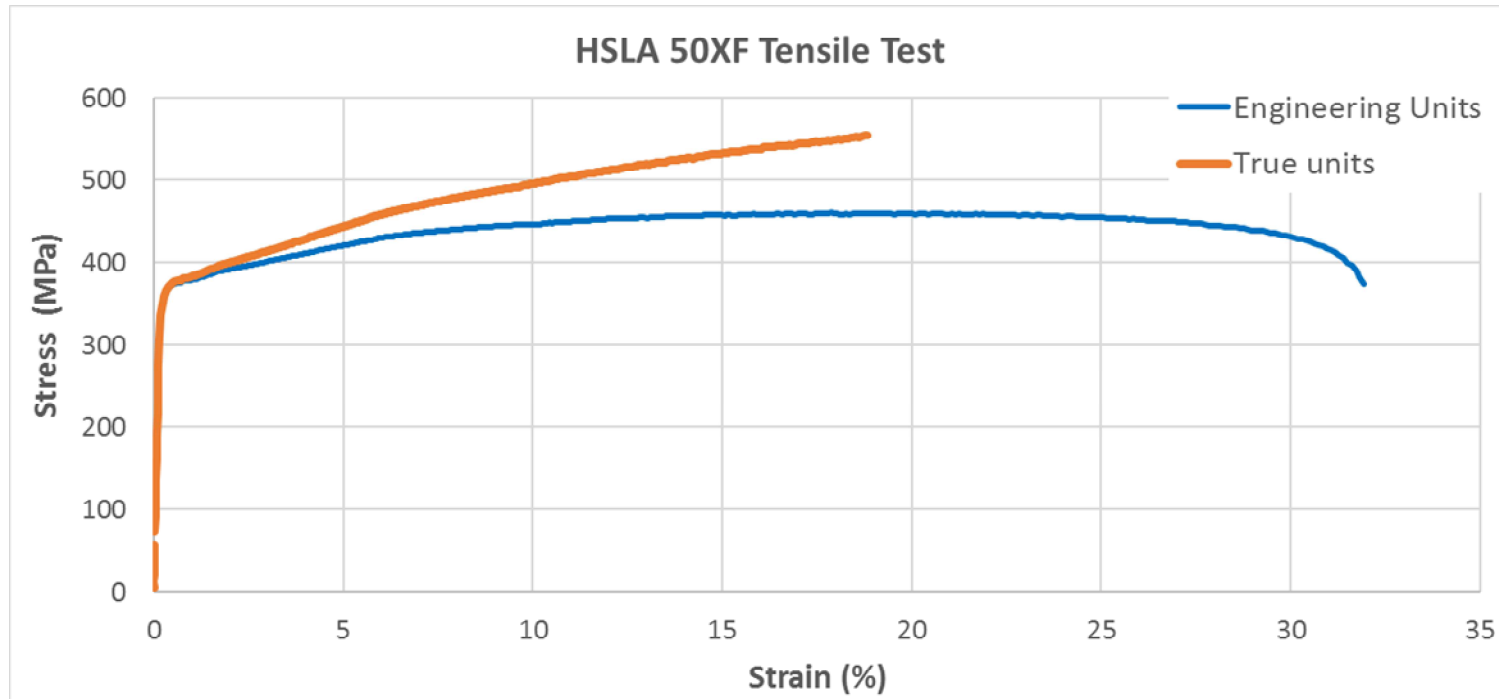
$$\sigma = s (1+e) \quad \epsilon = \ln (1+e)$$



# Engineering vs True

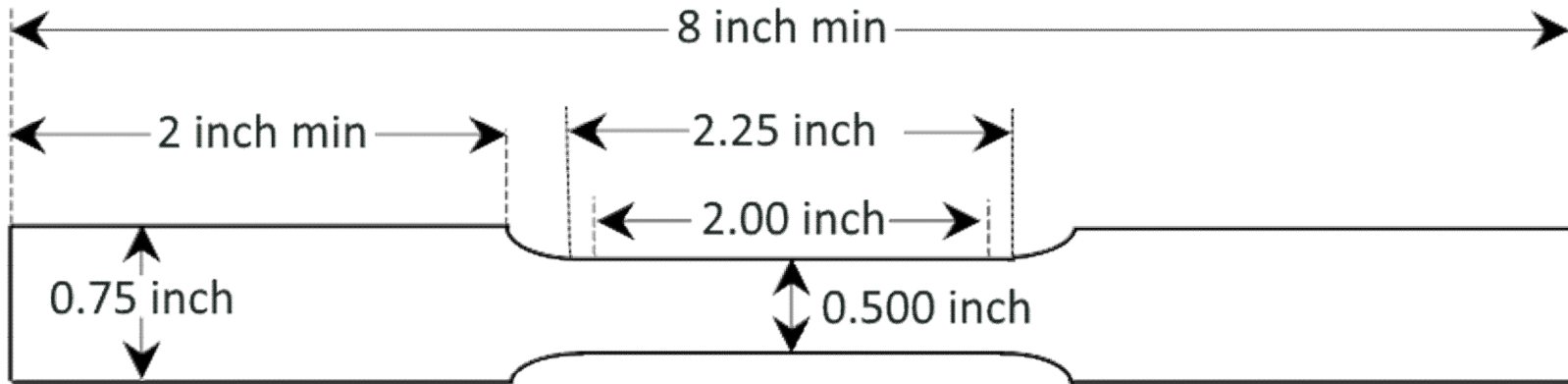
$$\sigma = s (1+e)$$

$$\epsilon = \ln (1+e)$$



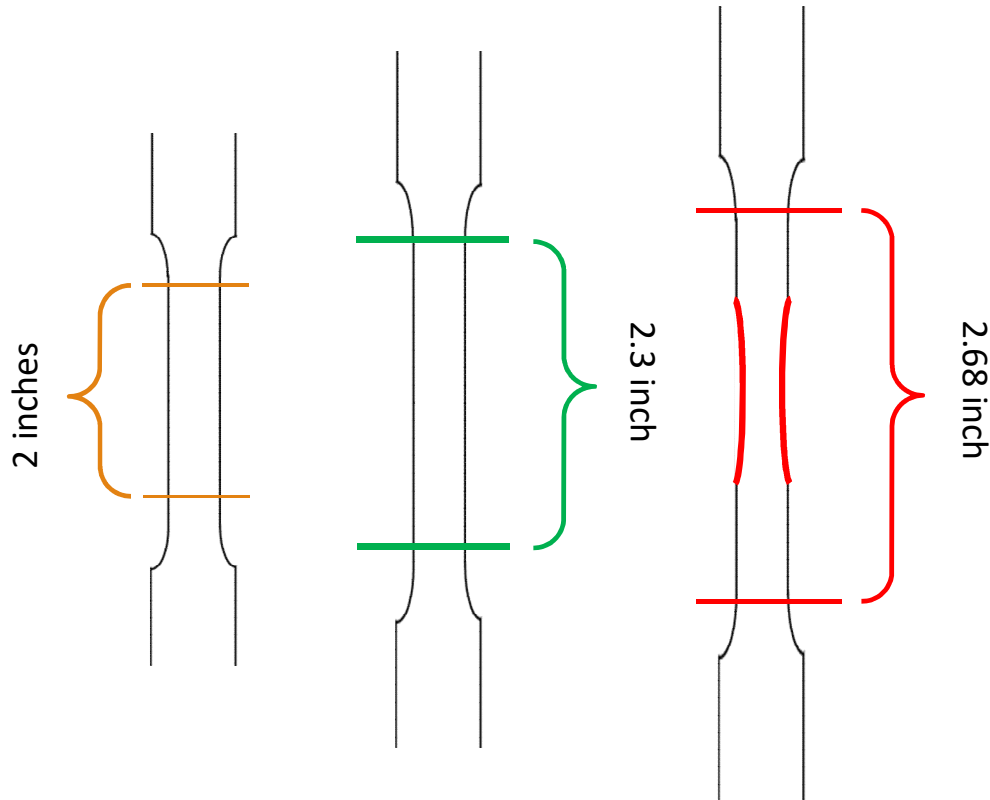


# ASTM Tensile Bar





# Calculating Elongation

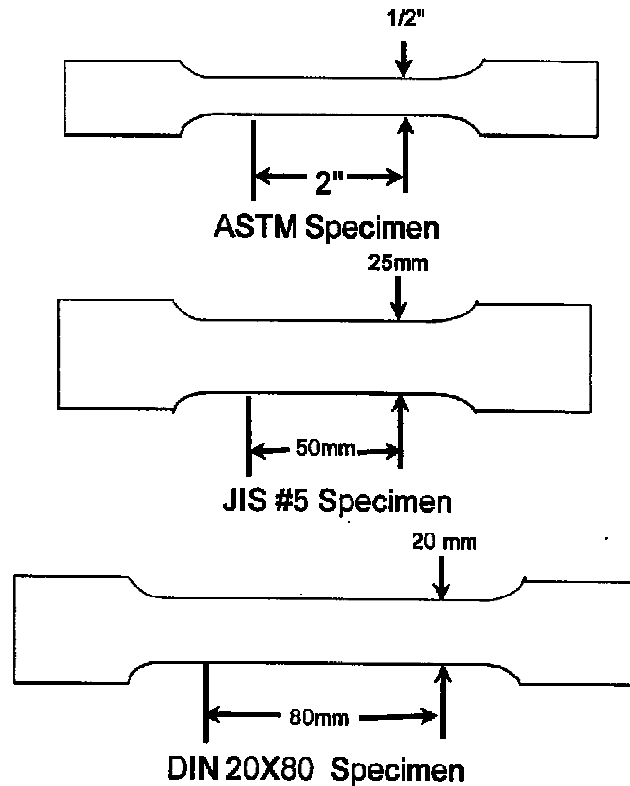


$$\frac{\Delta L}{L} = \frac{2.3 - 2}{2} = \frac{0.3}{2} = 0.15 = 15\%$$

$$\frac{\Delta L}{L} = \frac{2.68 - 2}{2} = \frac{0.68}{2} = 0.34 = 34\%$$



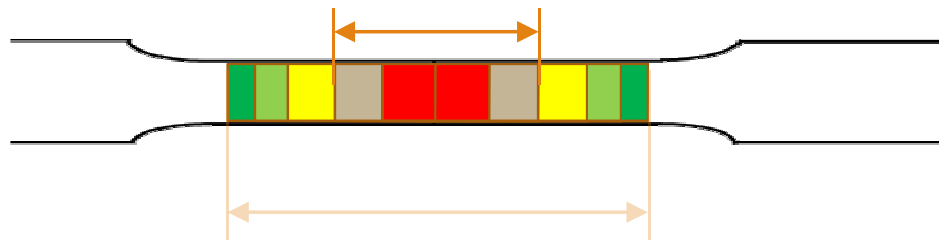
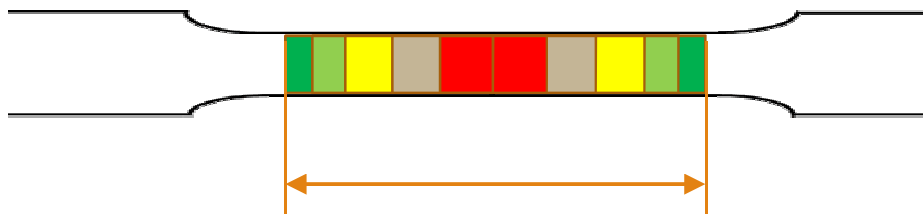
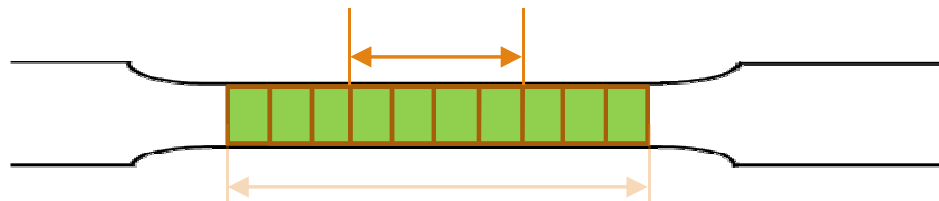
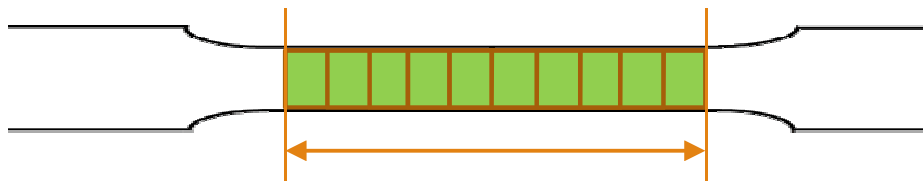
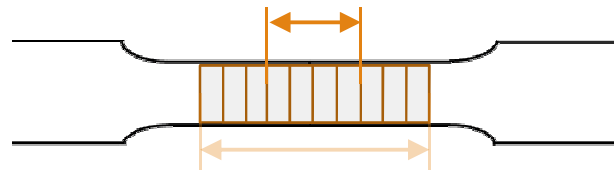
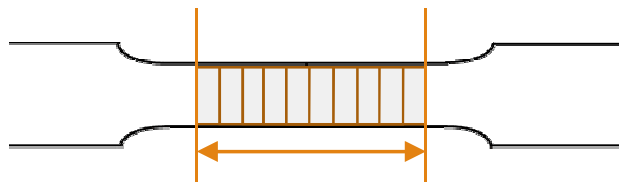
# Tensile Bar Specification





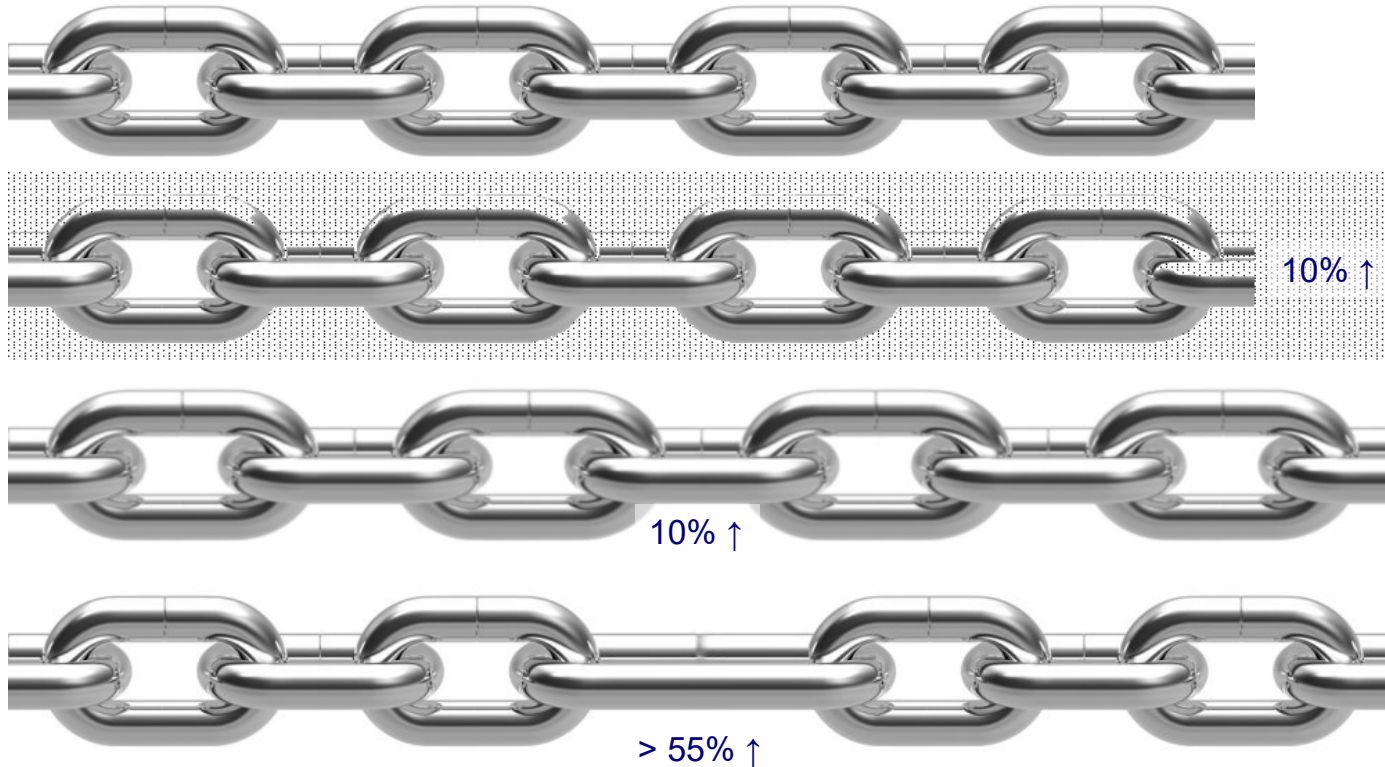


# Effect of Gauge Length



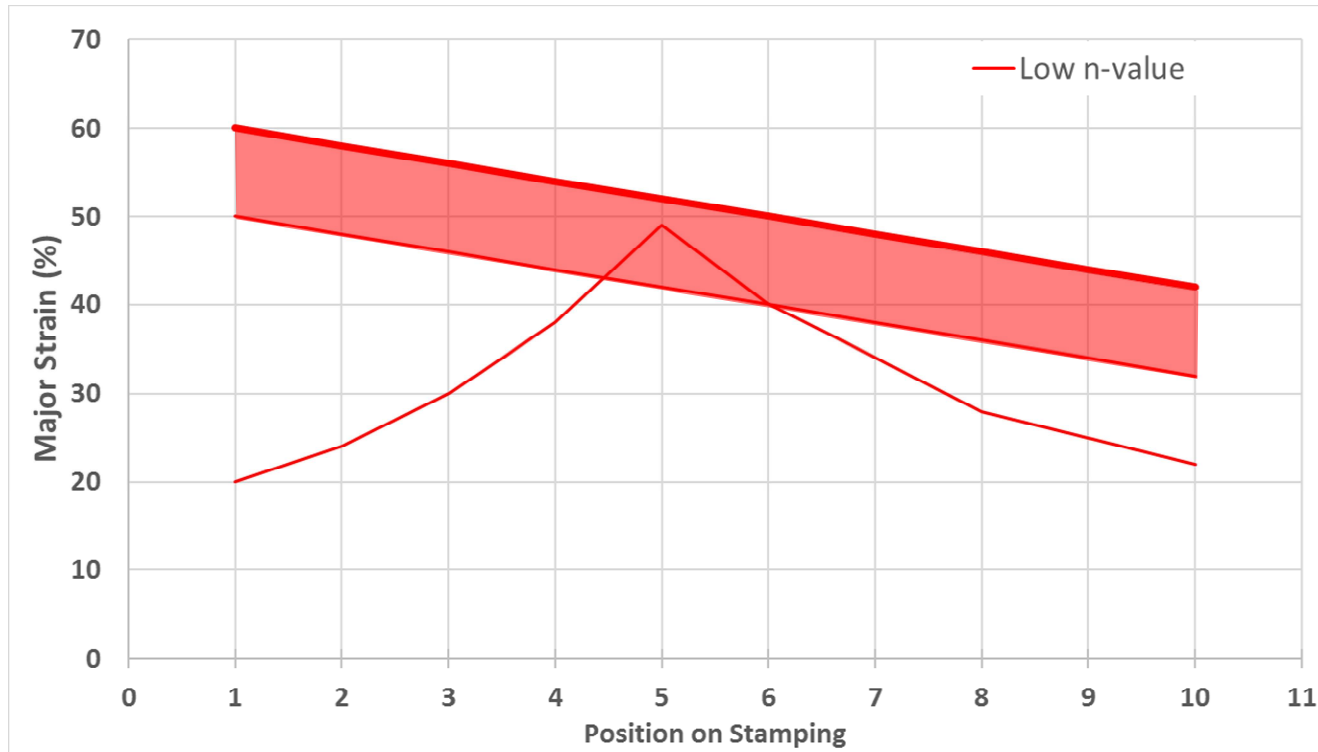


# ↑n-value means Better Ability to Distribute Strains



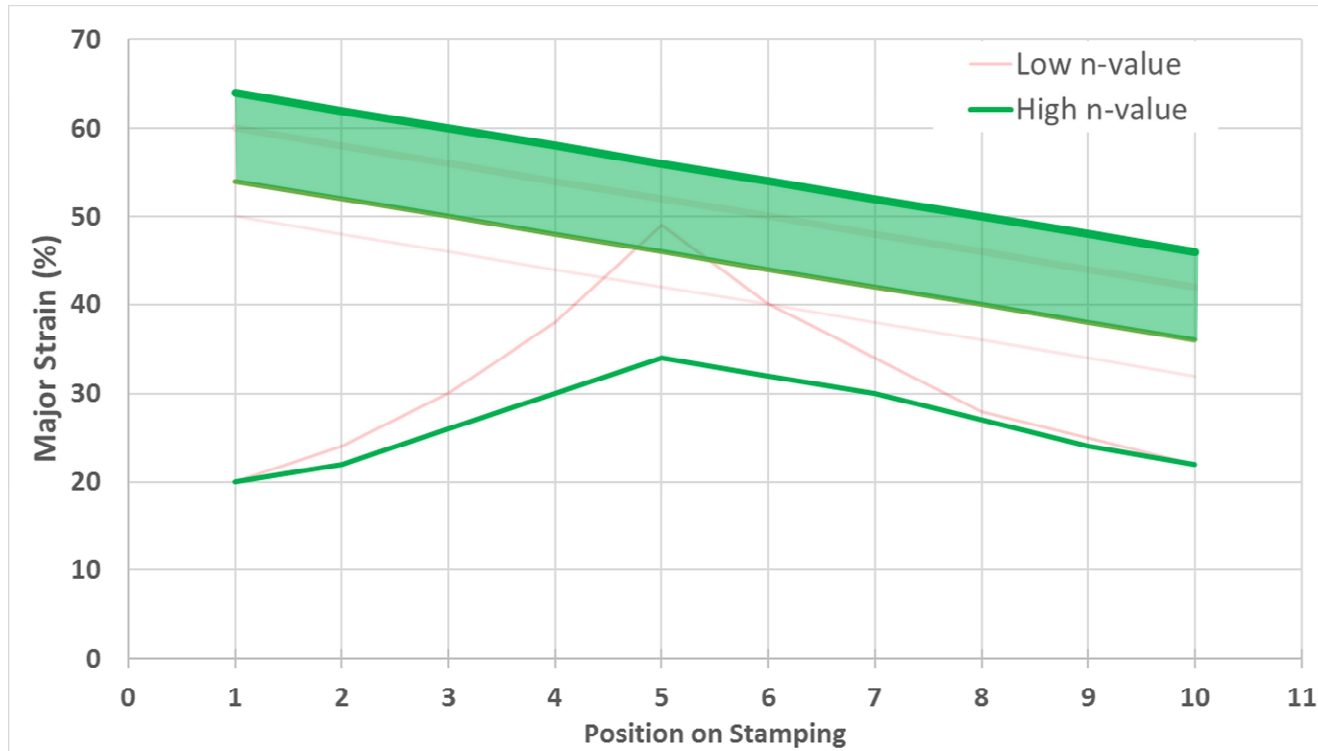


# N-Value



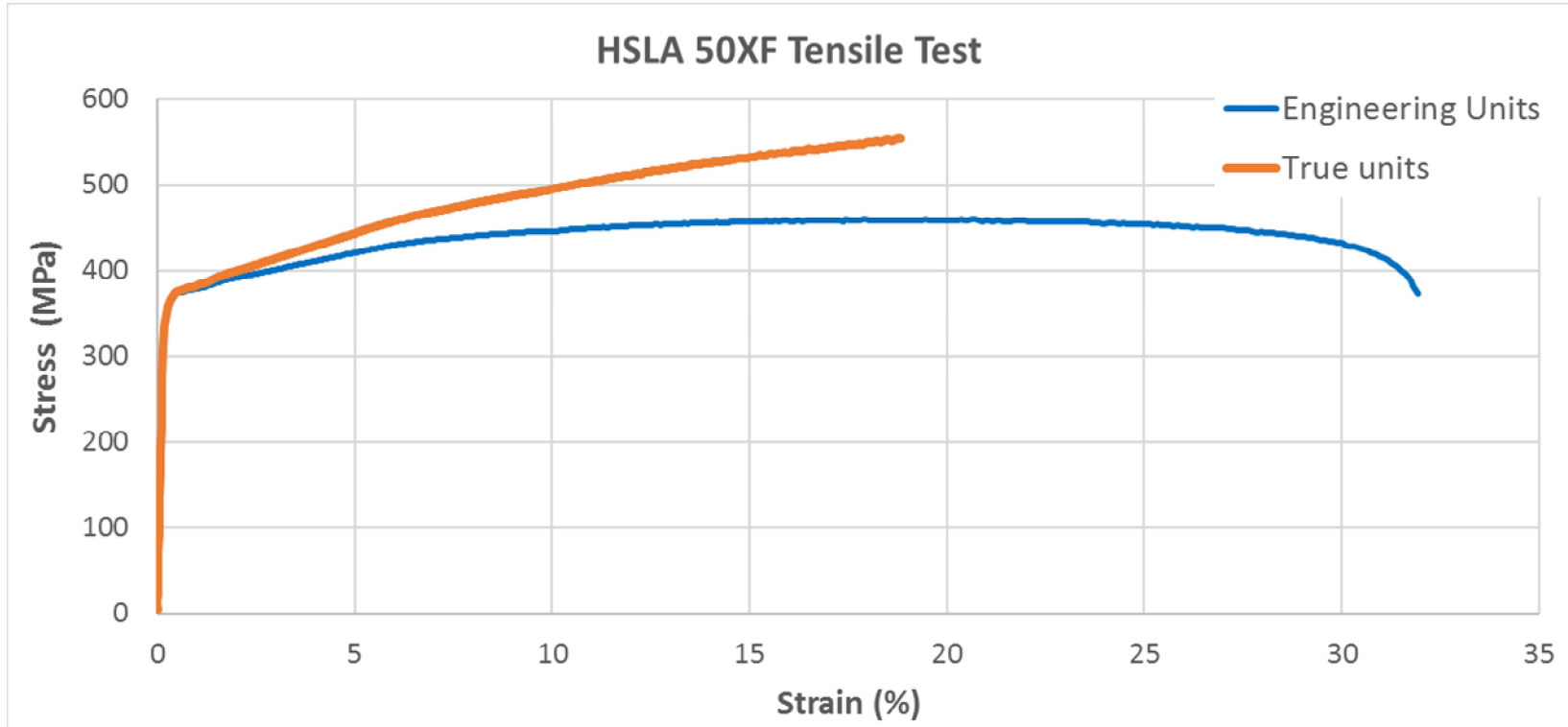


# N-Value





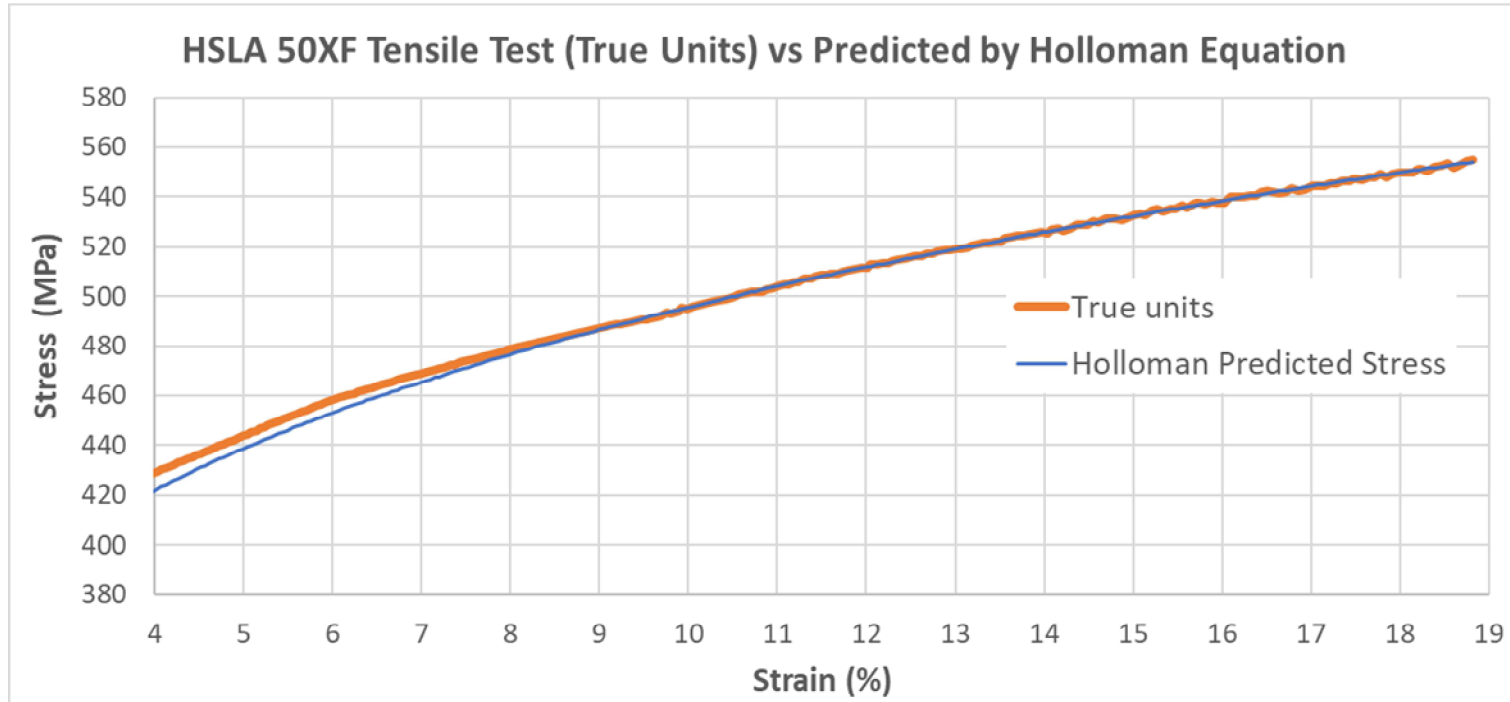
# Data Points from Tensile Testing





# Holloman Power Law: true stress-strain

$$\sigma = K\epsilon^n$$





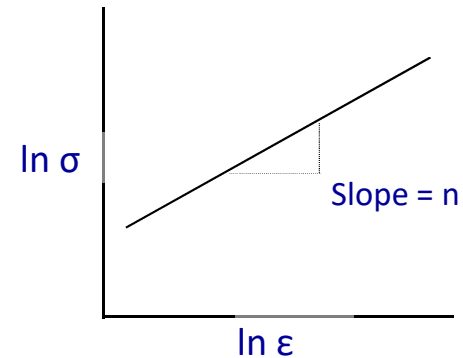
# Strain Hardening Exponent = N-Value

Holloman Power Law:

$$\sigma = K\varepsilon^n$$

$$\ln \sigma = \ln K + n(\ln \varepsilon)$$

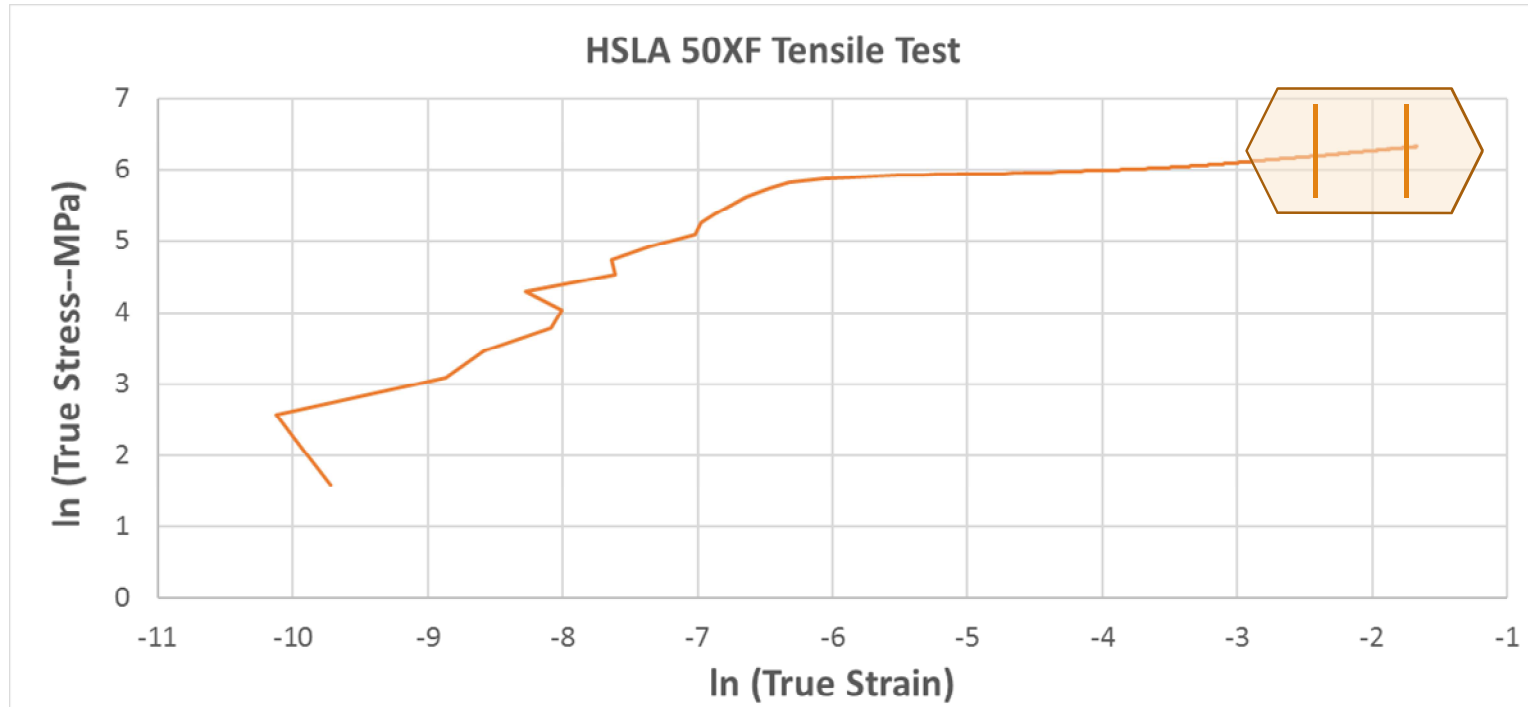
**n the slope of the  $\ln \sigma$  -  $\ln \varepsilon$  plot**





$$\sigma = K\varepsilon^n$$

$$\ln \sigma = \ln K + n(\ln \varepsilon)$$





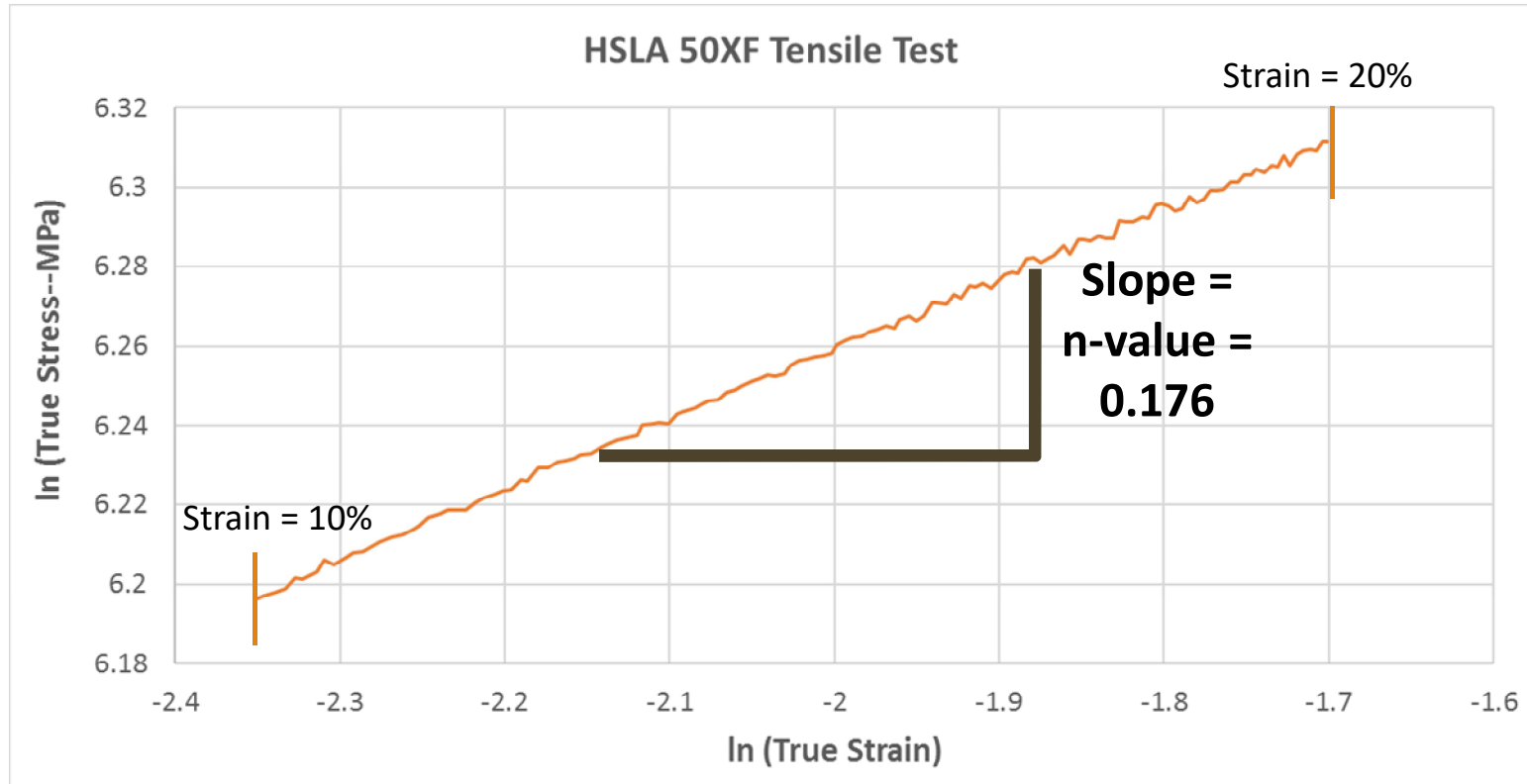


$$\sigma = K\varepsilon^n$$

$$K=743\text{MPa},$$

$$\ln\sigma = \ln K + n(\ln\varepsilon)$$

$$n=0.176$$



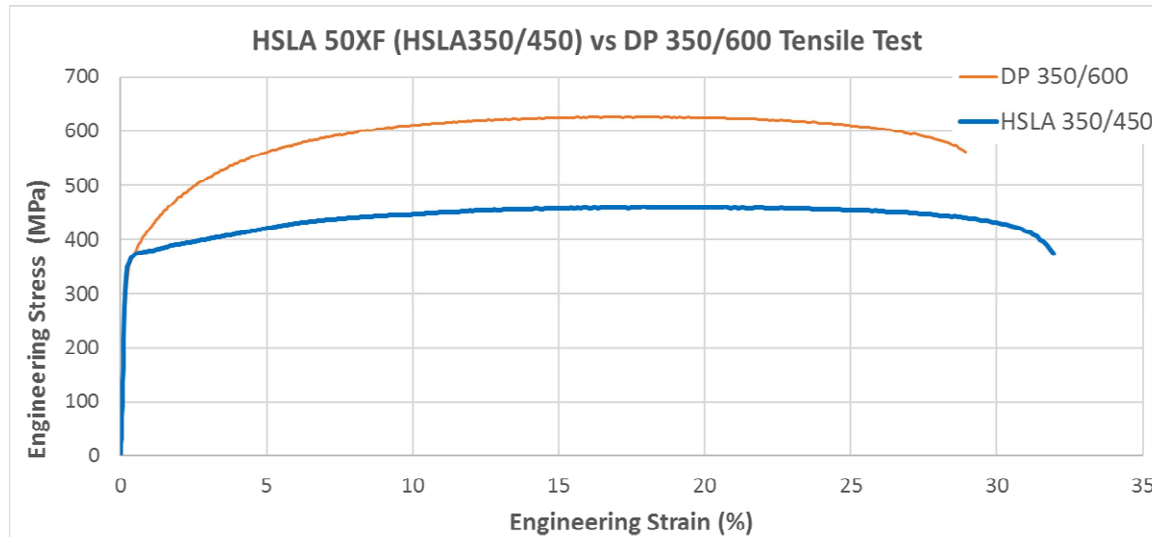


# Physical Meaning of N-value

Calculated as slope of the  $\ln \sigma - \ln \epsilon$  plot

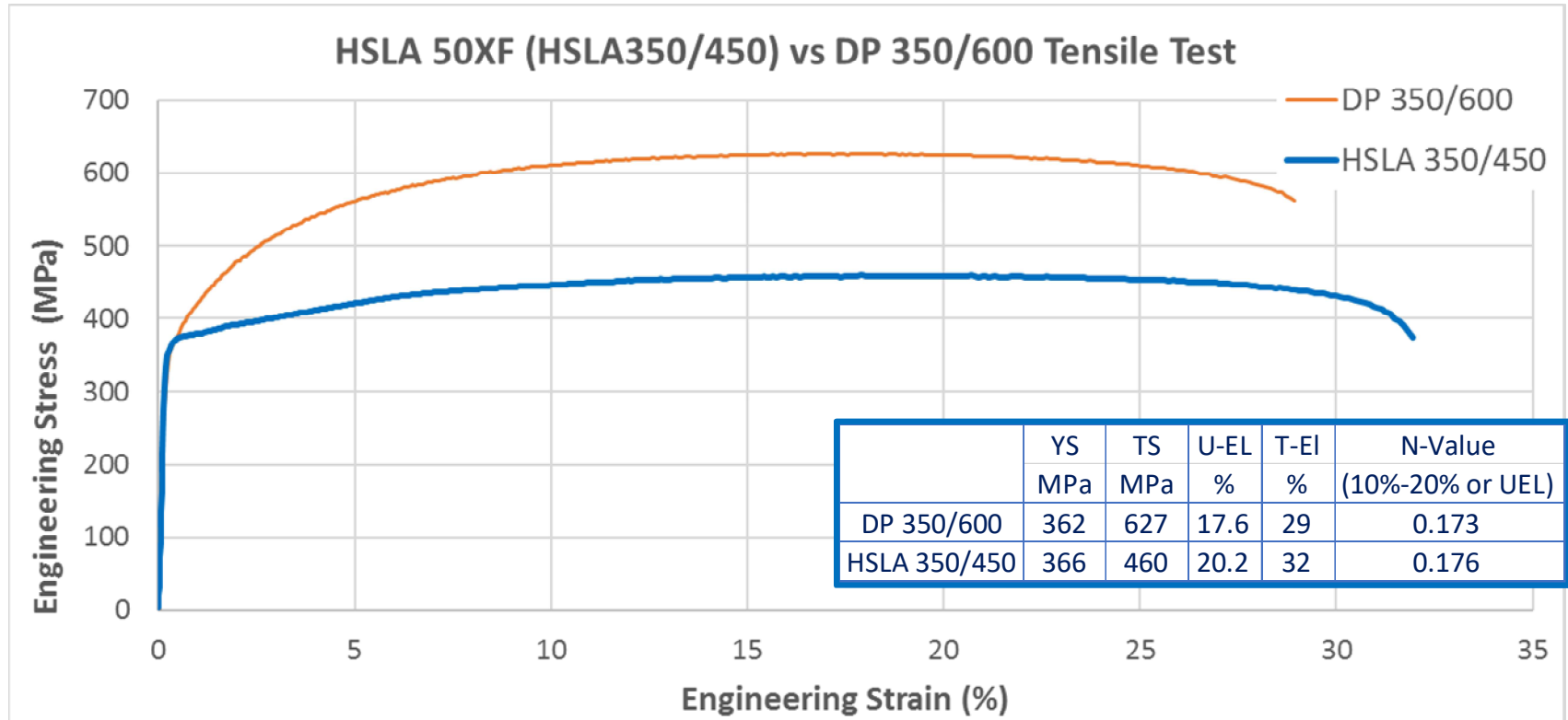
Higher slope = higher n-value

The larger the YS and TS gap, the better the formability.





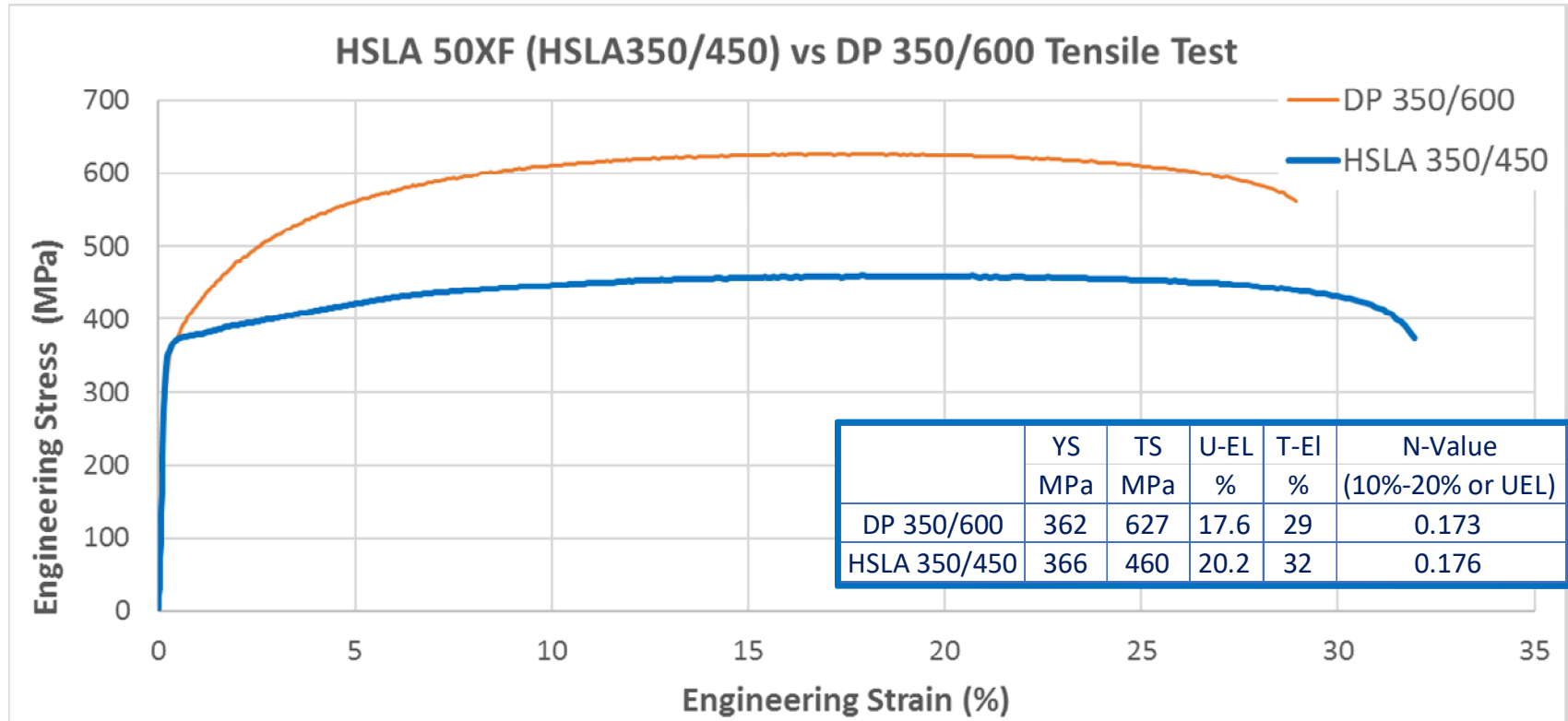
# Typical Stress-Strain Curves





With both having similar YS, EL, and n-value...

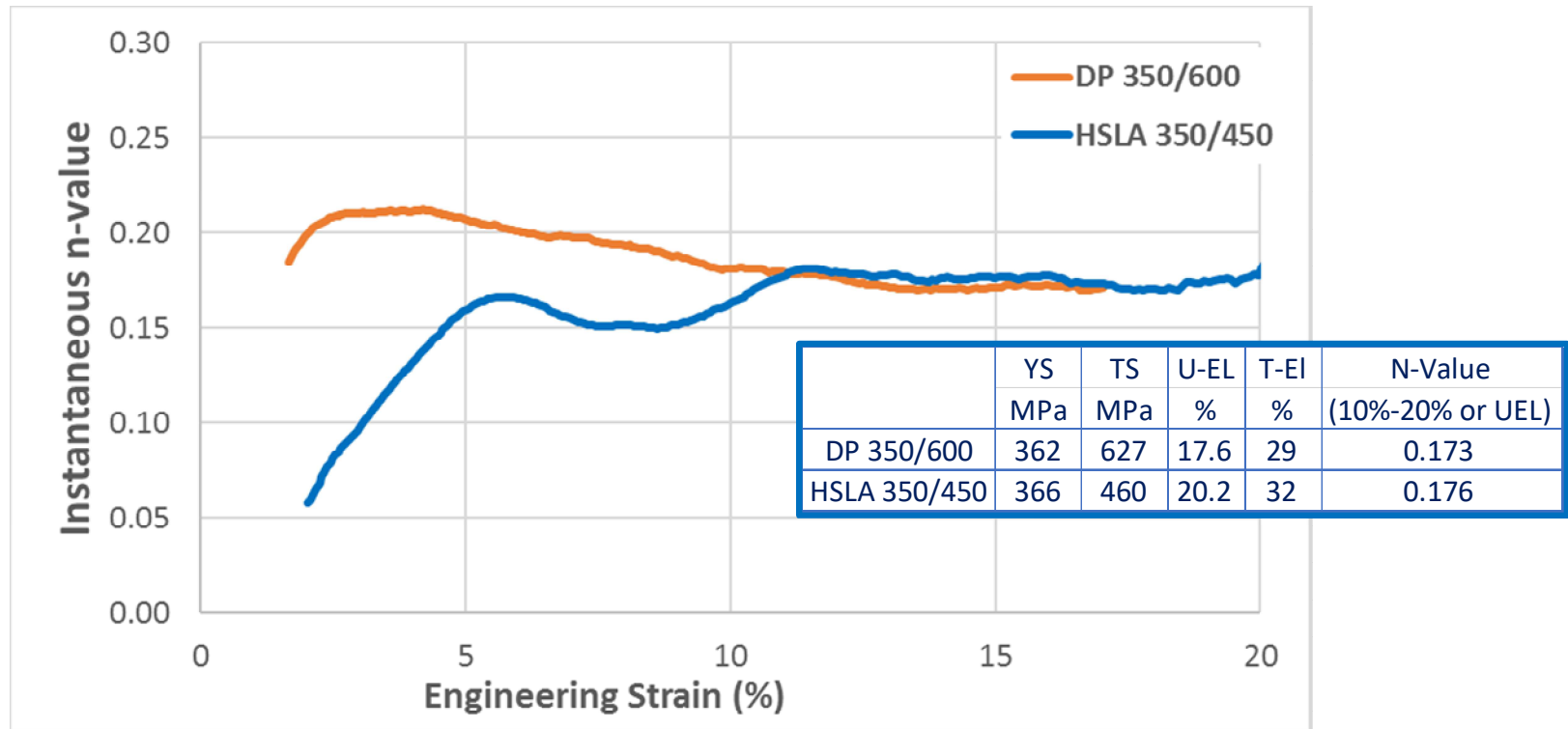
## Why does DP form better than HSLA?





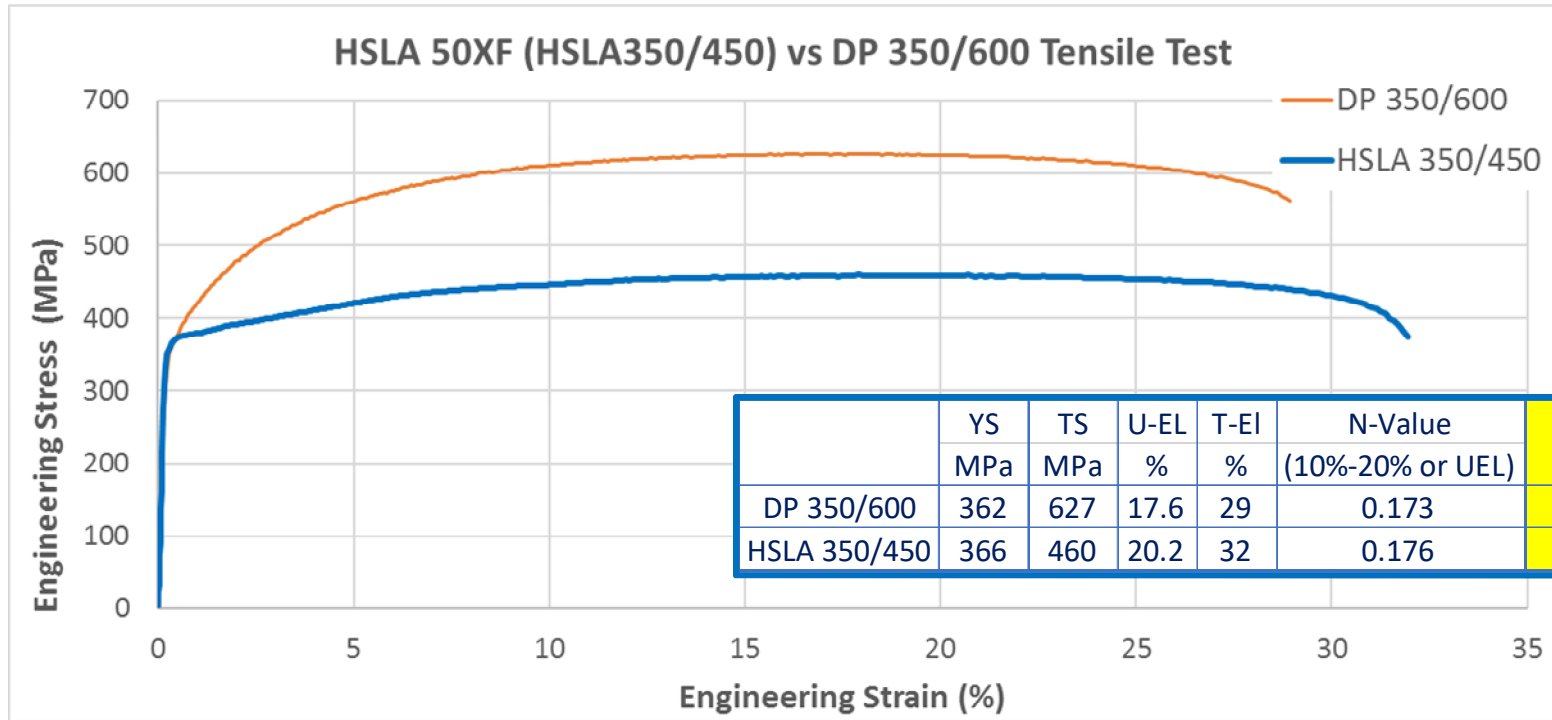
With both having similar YS, EL, and n-value...

## Why does DP form better than HSLA?





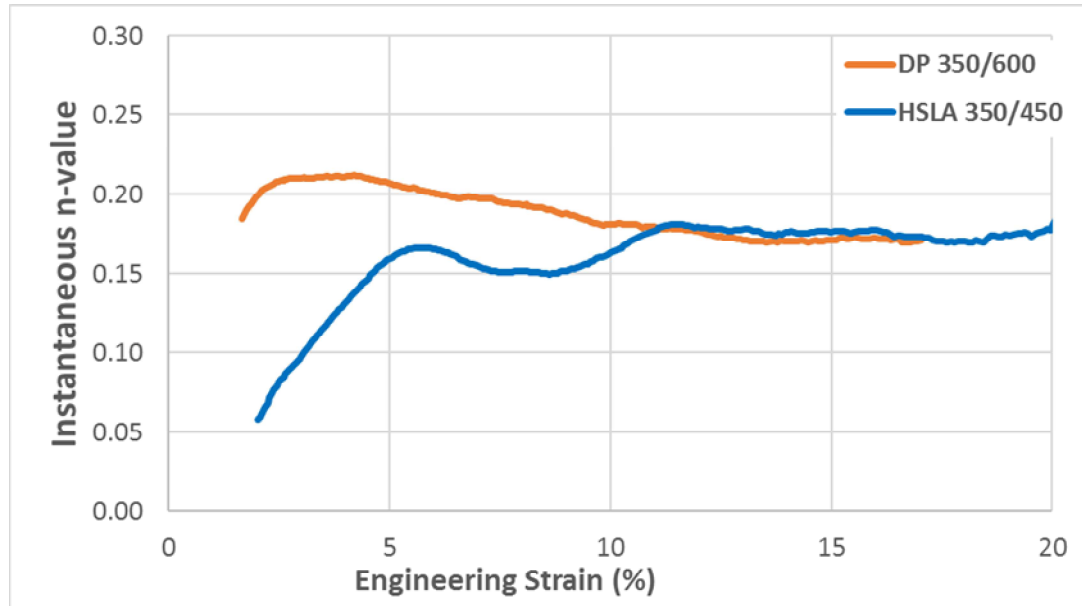
# Typical Stress-Strain Curves



High initial n-value reduces opportunities for strain localization and strain gradient formation



# Simulation Input?



Which n-value to use??

4% to 6%

6% to 12%

10% to 20%

10% to Uniform Elongation?



Plastic Strain Ratio  
Lankford Coefficient  
Plastic Anisotropy

r-value

Ratio of true width strain to true thickness strain  
in uniform elongation region

Higher r-value indicates better resistance to thinning



$$r = \frac{\epsilon_w}{\epsilon_t} = \left\{ \frac{\ln \frac{w}{w_0}}{\ln \frac{t}{t_0}} \right\}$$



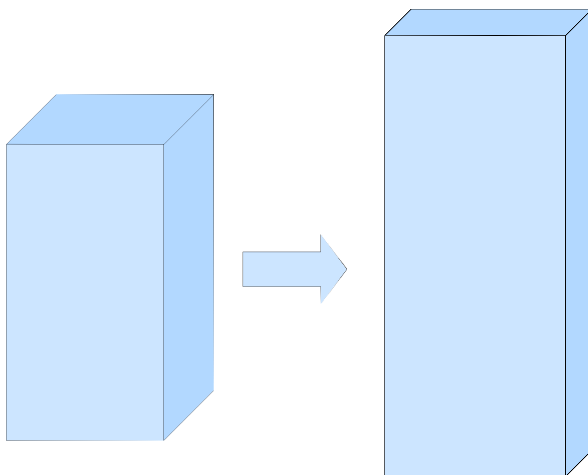


Plastic Strain Ratio  
Lankford Coefficient  
Plastic Anisotropy

r-value

Ratio of true width strain to true thickness strain  
in uniform elongation region

Low r-value  $\rightarrow$  width strain is small compared with thickness strain



Material with low r-value:  
longer and thinner  
after straining without much  
width change

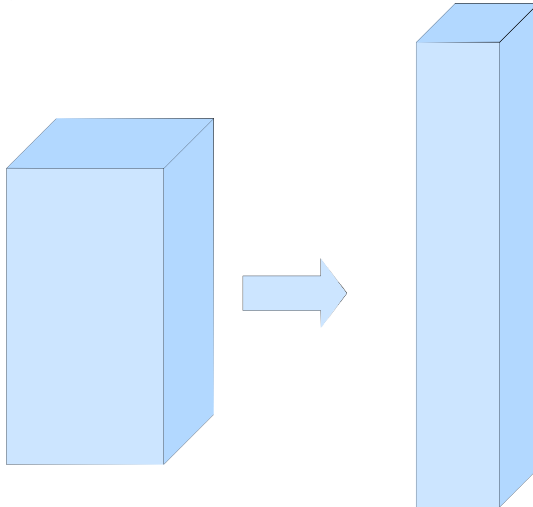


Plastic Strain Ratio  
Lankford Coefficient  
Plastic Anisotropy

# r-value

Ratio of true width strain to true thickness strain  
in uniform elongation region

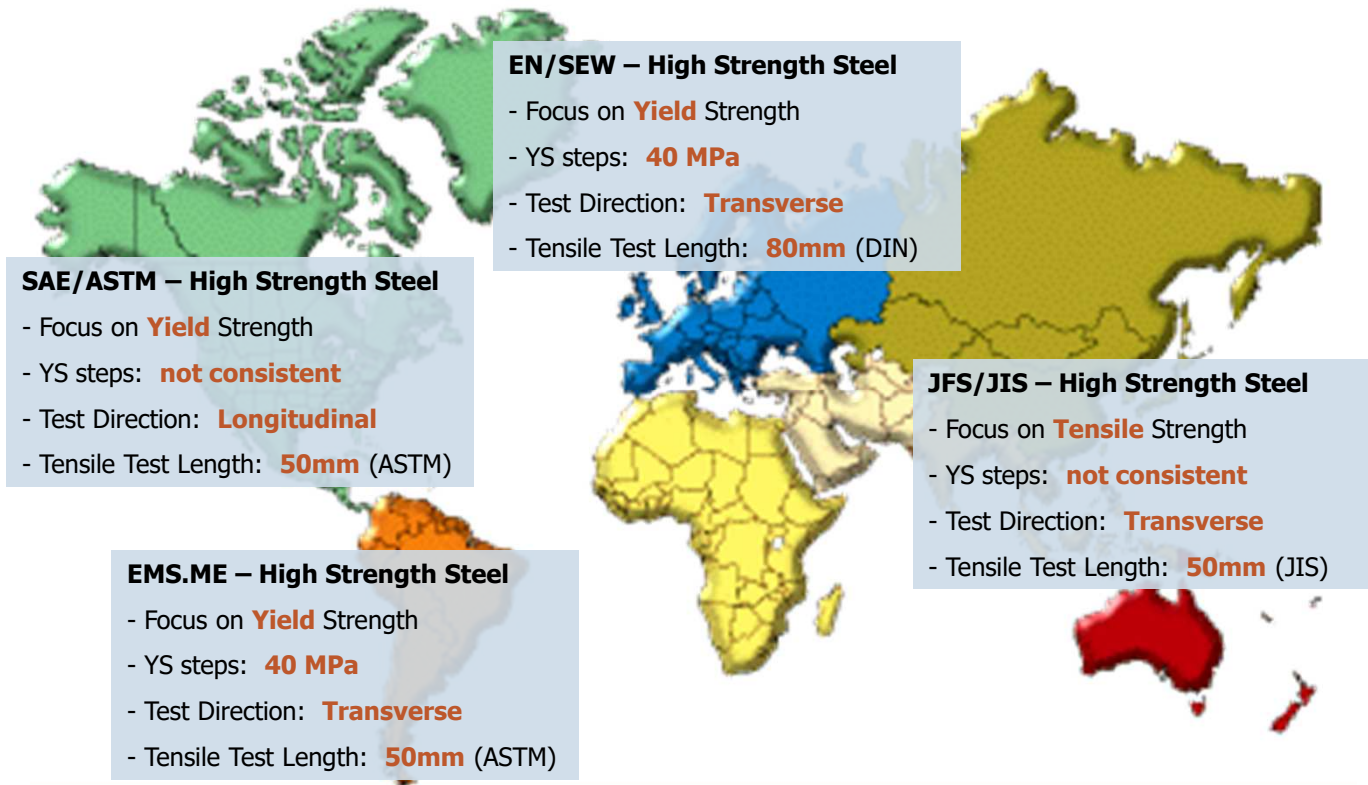
High r-value → width strain is large compared with thickness strain



Material with high r-value:  
longer and more narrow  
after straining without much  
thickness change



# Worldwide Specifications





# Strength Conversion

---

psi = pounds per square inch

ksi = kilo (thousand) pounds per square inch

MPa = mega Pascal = 1,000,000 Pascal

GPa = giga Pascal = 1,000 MPa

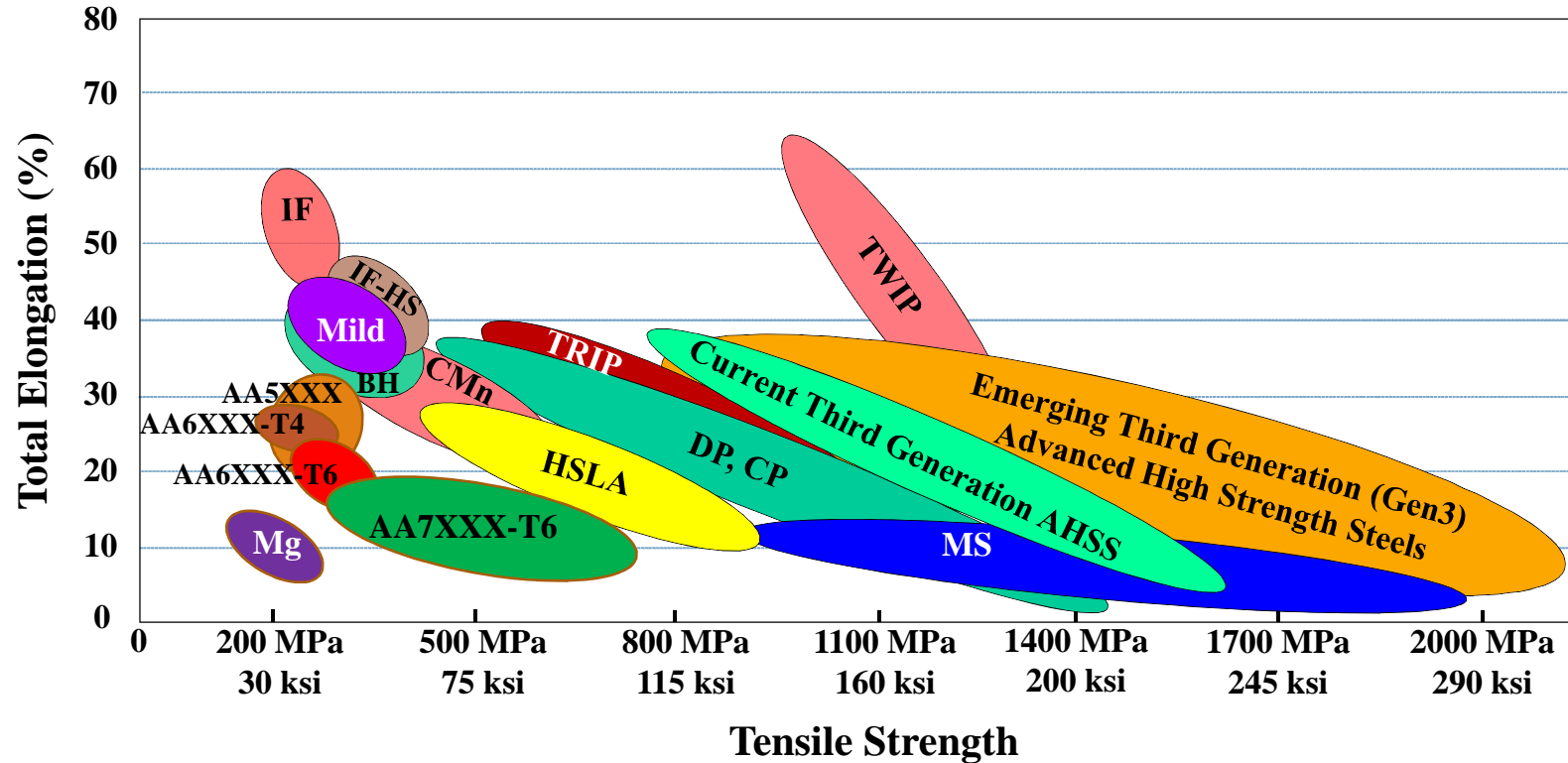
1 ksi = 6.895 MPa

1 ksi  $\approx$  7 MPa

HSLA 50XF = HSLA 350/450

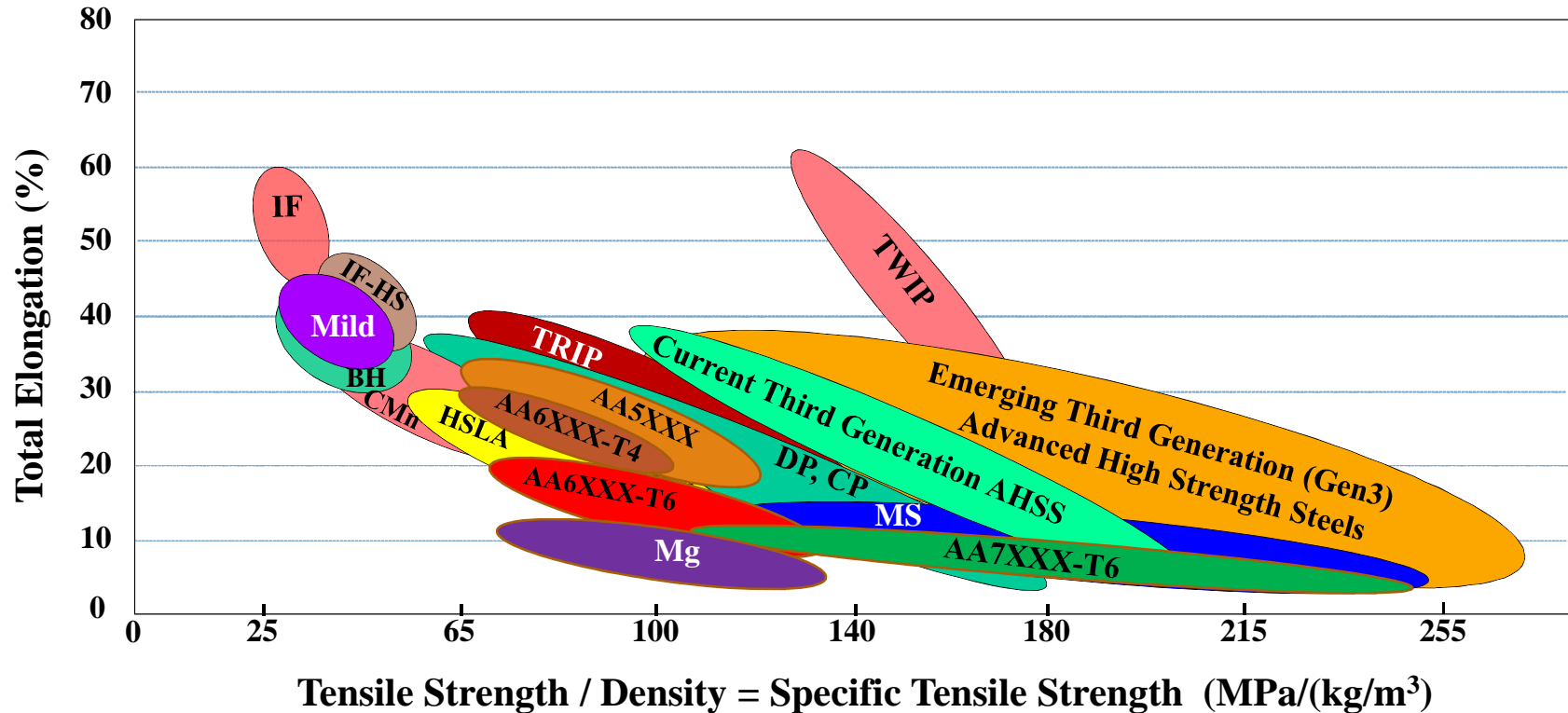


# Tensile Strength vs Elongation





# Specific Strength vs Elongation Effect of Density

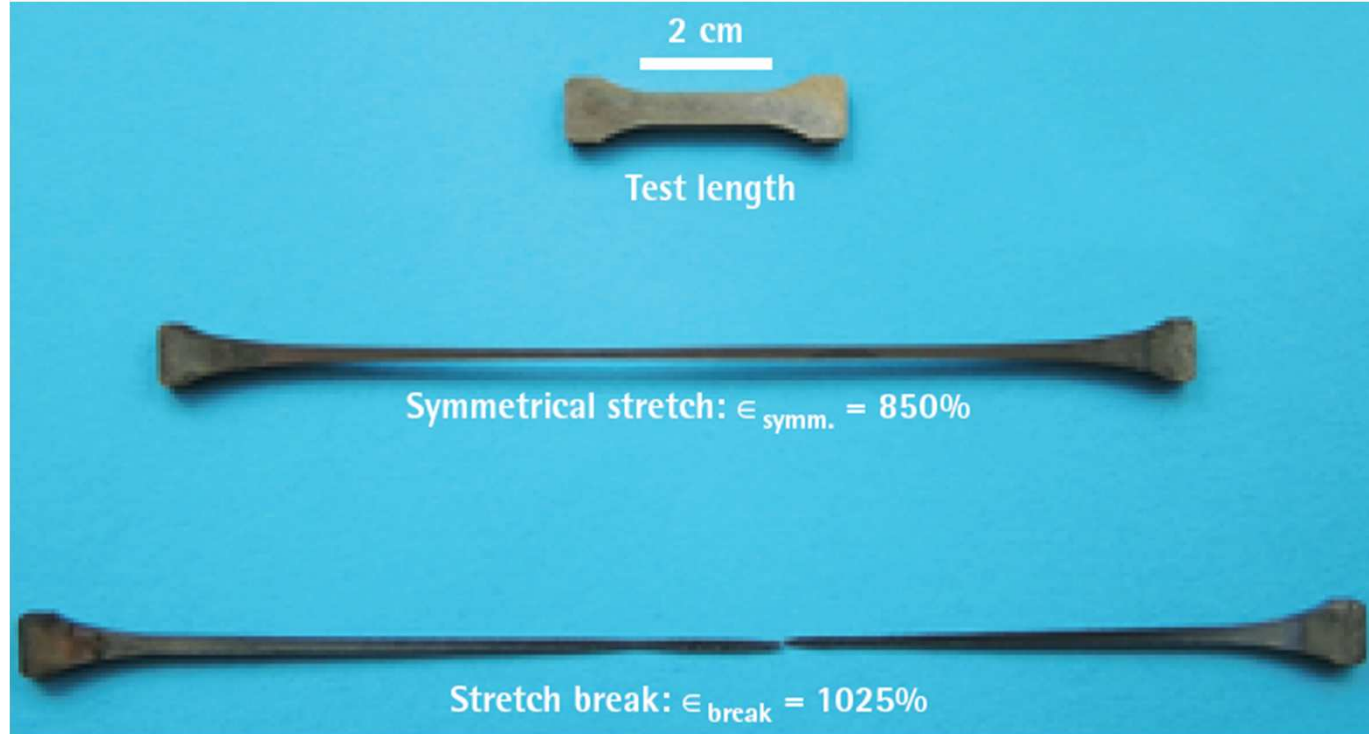




# TWIP: Twinning Induced Plasticity

X-IP™: Xtremely formable + Xtremely high strength steels with Induced Plasticity

[http://www.mpg.de/english/illustrationsDocumentation/multimedia/mpResearch/2004/heft04/4\\_04MPR\\_36\\_41.pdf](http://www.mpg.de/english/illustrationsDocumentation/multimedia/mpResearch/2004/heft04/4_04MPR_36_41.pdf)





For more information, please visit

[www.Learning4M.com](http://www.Learning4M.com)

Or write us at

[4M@Learning4M.com](mailto:4M@Learning4M.com)

Or

[EQS@EQSgroup.com](mailto:EQS@EQSgroup.com)